

2/PRTS

10/540628

NSC-M925

- 1 - JC09 Rec'd PCT/PTO 23 JUN 2005

DESCRIPTION

HIGH BURRING, HIGH STRENGTH STEEL SHEET EXCELLENT IN  
SOFTENING RESISTANCE OF WELD HEAT AFFECTED ZONE AND  
5 METHOD OF PRODUCTION OF SAME

TECHNICAL FIELD

The present invention relates to high burring, high  
strength steel sheet having a tensile strength of 540 MPa  
10 or more excellent in softening resistance of the weld  
heat affected zone and a method of production of the  
same, more particularly relates to high burring, high  
strength steel sheet excellent in softening resistance of  
the weld heat affected zone suitable as a material used  
15 for applications such as auto parts where both  
workability and weld zone strength are sought in the case  
of spot, arc, plasma, laser, or other welding after being  
formed or in the case of being formed after such welding  
and a method of production of the same.

20 BACKGROUND ART

In recent years, for lightening weight for improving  
the fuel efficiency of automobiles etc., Al alloys and  
other light metals or high strength steel sheet have been  
increasingly used for auto parts and members.

25 However, Al alloys and other light metals have the  
advantage of being high in relative strength, but are  
remarkably higher in price compared with steel, so their  
use has been limited to specialty applications. To  
promote reduction of the weight of automobiles in a  
30 broader area, use of inexpensive high strength steel  
sheet is being strongly sought.

In general, materials become worse in formability  
the higher the strength. Ferrous metal materials are no  
exception. Attempts have been made to achieve both high  
35 strength and high ductility up until now. Further,  
another characteristic sought in a material used for auto  
parts is, in addition to ductility, burring. However,

burring also exhibits a tendency to fall along with higher strength, so the improvement of burring is also becoming a topic in use of high strength steel sheet for auto parts. On the other hand, auto parts are comprised of press formed and other worked members assembled together by spot, arc, plasma, laser, and other welding. Further, recently, steel sheet has been welded together, then press formed in some cases. Whatever the case, the weld strength at the time of forming or the time of use assembled as a part is extremely important from the viewpoints of the forming limits and safety. Therefore, in application of high strength steel sheet to auto parts etc., the burring and the weld zone strength also become important issues for study.

For high strength steel sheet excellent in burring, an invention adding Ti and Nb to reduce the second phase and cause precipitation strengthening by TiC and NbC in the main phase of polygonal ferrite so as to obtain high strength rolled steel sheet excellent in stretch flange formability has been proposed (Japanese Unexamined Patent Publication (Kokai) No. 6-200351).

Further, an invention adding Ti and Nb so as to reduce the second phase, make the microstructure acicular ferrite, and cause precipitation strengthening by TiC and NbC to obtain high strength, hot rolled steel sheet excellent in stretch flange formability has also been proposed (Japanese Unexamined Patent Publication (Kokai) No. 7-11382).

On the other hand, as technology for improving the weld zone strength, an invention complexly adding Nb and Mo so as to suppress the softening of the weld zone in steel sheet has been proposed (Japanese Unexamined Patent Publication (Kokai) No. 2000-87175).

Further, an invention making active use of the precipitation of NbN to suppress softening of the weld zone so as to obtain steel sheet comprised of ferrite and martensite has also been proposed (Japanese Unexamined

Patent Publication (Kokai) No. 2000-178654).

However, in suspension arms, front side members, and steel sheet for other parts, burring and other formability and the strength of the weld zone are very important. In the above prior art, the two characteristics could never simultaneously be satisfied. Further, for example, even if the two characteristics are satisfied, provision of a method of production enabling production inexpensively and safely is important. The above prior art must be said to be insufficient.

That is, in the invention described in Japanese Unexamined Patent Publication (Kokai) No. 6-200351, to obtain a high stretch flange formability, an area ratio of at least 85% of polygonal ferrite is essential, but to obtain a 85% or higher polygonal ferrite, the steel has to be held for a long time to promote the growth of the ferrite grains after hot rolling. This is not preferable in operating costs.

Further, in the invention described in Japanese Unexamined Patent Publication (Kokai) No. 7-11382, due to the microstructure with the high dislocation density and the precipitation of fine TiC and/or NbC, just a ductility of about 17% at 80 kgf/mm<sup>2</sup> is obtained and the formability is insufficient.

Further, these inventions do not allude at all to softening of the weld zone. On the other hand, the invention described in Japanese Unexamined Patent Publication (Kokai) No. 2000-87175 does not describe anything regarding the improvement of burring.

Further, the invention described in Japanese Unexamined Patent Publication (Kokai) No. 2000-178654 relates to a complex ferrite-martensite structure steel, which is clearly different from the technology of the present invention for obtaining a microstructure of steel sheet excellent in burring.

#### DISCLOSURE OF THE INVENTION

The present invention solves these problems and

provides high burring, high strength steel sheet  
excellent in softening resistance of the weld heat  
affected zone suitable as a material for use in  
applications such as auto parts where both workability  
5 and weld zone strength are demanded in the case of spot,  
arc, plasma, laser, or other welding after being formed  
or the case of being formed after welding, and a method  
of production of the same. That is, the present invention  
has as its object the provision of high burring, high  
10 strength steel sheet having a tensile strength of 540 MPa  
or more excellent in softening resistance of the weld  
heat affected zone and a method of production enabling  
that steel sheet to be produced inexpensively and stably.

The inventors kept in mind the process of production  
15 of thin steel sheet being produced on an industrial scale  
by production facilities currently ordinarily employed  
and engaged in intensive studies to improve the softening  
resistance of the weld heat affected zone of high  
burring, high strength steel sheet. As a result, they  
20 discovered that high burring, high strength steel sheet  
containing C: 0.01 to 0.1%, Si: 0.01 to 2%, Mn: 0.05 to  
3%,  $P \leq 0.1\%$ ,  $S \leq 0.03\%$ , Al: 0.005 to 1%, N: 0.0005 to 0.005%,  
and Ti: 0.05 to 0.5%, further containing C, S, N, and Ti  
in ranges satisfying  $0 < C - (12/48Ti - 12/14N - 12/32S) \leq 0.05\%$ ,  
25  $Mo + Cr \geq 0.2\%$ ,  $Cr \leq 0.5\%$ , and  $Mo \leq 0.5\%$ , the balance comprising  
Fe and unavoidable impurities, and having a  
microstructure comprised of ferrite or ferrite and  
bainite, is extremely excellent in burring, but has a  
weld heat affected zone which remarkably softens.  
30 Further, they pinpointed the cause of the softening of  
the weld heat affected zone of said high burring, high  
strength steel sheet as being the tempering of the  
microstructure due to the welding thermal history and  
newly discovered that to improve the softening  
35 resistance, complex addition of Cr and Mo was extremely  
effective, and thereby completed the present invention.

That is, the gist of the present invention is as follows:

(1) High burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone characterized by containing, by wt%, C: 5 0.01 to 0.1%, Si: 0.01 to 2%, Mn: 0.05 to 3%,  $P \leq 0.1\%$ ,  $S \leq 0.03\%$ , Al: 0.005 to 1%, N: 0.0005 to 0.005%, and Ti: 0.05 to 0.5% and further containing C, S, N, Ti, Cr, and Mo in ranges satisfying  $0 < C - (12/48Ti - 12/14N - 12/32S) \leq 0.05\%$  and  $Mo + Cr \geq 0.2\%$ ,  $Cr \leq 0.5\%$ , and  $Mo \leq 0.5\%$ , the balance 10 comprising Fe and unavoidable impurities, wherein the microstructure is comprised of ferrite or ferrite and bainite.

(2) High burring, high strength steel sheet excellent in softening resistance of the weld heat 15 affected zone characterized in that said steel further contains, by wt%, Nb: 0.01 to 0.5% and further contains Nb in a range satisfying  $0 < C - (12/48Ti - 12/93Nb - 12/14N - 12/32S) \leq 0.05\%$ , the balance comprising Fe and unavoidable impurities.

(3) High burring, high strength steel sheet excellent in softening resistance of the weld heat 20 affected zone as set forth in (1) or (2), characterized by further containing, by wt%, one or two of Ca: 0.0005 to 0.002%, a REM: 0.0005 to 0.02%, Cu: 0.2 to 1.2%, Ni: 25 0.1 to 0.6%, and B: 0.0002 to 0.002%.

(4) High burring, high strength steel sheet excellent in softening resistance of the weld heat 30 affected zone as set forth in any one of (1) to (3), characterized by being automotive thin steel sheet coated with zinc.

(5) A method of production of high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone characterized by hot rolling a slab having the ingredients for obtaining the thin 35 steel sheet as set forth in any one of (1) to (3) at which time ending finish rolling at a temperature region

of the  $Ar_3$  transformation point temperature + 30°C or more, then cooling within 10 seconds by a cooling rate of an average cooling rate until the end of cooling of 50°C/sec or more until a temperature region of 700°C or less, and coiling at a coiling temperature of 350°C to 650°C.

(6) A method of production of high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone characterized by hot rolling a slab having the ingredients for obtaining the thin steel sheet as set forth in any one of (1) to (3), pickling it, cold rolling it, then holding it at a temperature region of 800°C or more for 5 to 150 seconds, then cooling it by a cooling rate of an average cooling rate of 50°C/sec or more until a temperature region of 700°C or less as a heat treatment process.

(7) A method of production of high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone as set forth in (5), characterized by dipping the steel sheet in a zinc coating bath after the end of the hot rolling process to coat the surface with zinc.

(8) A method of production of high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone as set forth in (6), characterized by dipping the steel sheet in a zinc coating bath after the end of the heat treatment process to coat the surface with zinc.

(9) A method of production of high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone as set forth in (7) or (8), characterized by alloying after dipping the steel sheet in a zinc coating bath for coating zinc.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a view of the relationship between the amount of  $C^*$  and amount of Cr+Mo and the softening degree

$\Delta H_v$  of the weld heat affected zone.

FIG. 2 is a view of the relationship with the hardness of the arc weld zone for steel sheets of compositions with amounts of  $C^*$  and amounts of Cr+Mo changed.

Fig. 3(a) is a plan view of the test piece of the hot-rolled steel sheet according to JIS Z 2201 under the test method of JIS Z 2241, and Fig. 3(b) is a side view of this test piece.

#### BEST MODE FOR WORKING THE INVENTION

First, the inventors investigated the effects on the softening resistance of the weld heat affected zone exerted by the amount of  $C^*$  ( $C^* = C - (12/48Ti - 12/14N - 12/32S)$ , hereinafter referred to as " $C^*$ ") and the Cr and Mo contents. The test materials for this were prepared as follows. That is, the inventors hot rolled slabs comprised of basically 0.05%C-1.0%Si-1.4%Mn-0.01%P-0.001%S and adjusted in ingredients to change the amount of  $C^*$  (Ti and N content) and amount of Cr+Mo, coiled them at ordinary temperature, held them at 550°C for 1 hour, then furnace cooled them as heat treatment. The inventors measured the hardnesses of the arc weld zones of these steel sheets. The results are shown in FIG. 2.

Here, from these results, the inventors newly discovered that the amount of  $C^*$  and amount of Cr+Mo are strongly correlated with the softening degree  $\Delta H_v$  of the weld heat affected zone ( $\Delta H_v$  defined as  $H_v$  (average value of matrix hardness) -  $H_v$  (hardness of weld heat affected zone): see FIG. 1) and that when the amount of  $C^*$  is 0 to 0.05% and the amount of Cr+Mo is 0.2% or more, the softening of the weld heat affected zone is remarkably suppressed.

This mechanism is not necessarily clear, but a material obtaining strength by a bainitic microstructure sometimes softens at the heat affected zone in an arc welding or other welding thermal cycle. It is believed

that Mo or Cr clusters or precipitates with C and other elements even in welding or another short thermal cycle so as to raise the strength and as a result suppresses the softening of the heat affected zone. However, with a  
5 total of the contents of Mo and Cr of less than 0.2%, the effect is lost.

On the other hand, to obtain Mo or Cr carbides etc., at least the equivalent of C fixed by TiC or other carbides precipitating at a high temperature must be  
10 contained. Therefore, with  $C^* \leq 0$ , this effect is lost.

Note that for measurement of the hardness of the weld heat affected zone of arc welding, a No. 1 test piece described in JIS Z 3101 was measured in accordance with the test method described in JIS Z 2244. However,  
15 the arc welding was performed with a shield gas of CO<sub>2</sub>, a wire of YM-60C,  $\phi 1.2$  mm made by Nippon Steel Welding Products and Engineering Co., Ltd., a welding rate of 100 cm/min, a welding current of  $260 \pm 10$  A, a welding voltage of  $26 \pm 1$  V, a thickness of the test material of 2.6 mm, a  
20 hardness measurement position of 0.25 mm from the surface, a measurement distance of 0.5 mm, and a test force of 98 kN.

Next, the microstructure of the steel sheet in the present invention will be explained.

25 The microstructure of the steel sheet is preferably a single phase of ferrite to secure superior burring. However, in accordance with need, the inclusion of some bainite is allowed, but to secure good burring, a volume fraction of bainite of 10% or less is preferable. Note  
30 that the "ferrite" referred to here includes bainitic ferrite and acicular ferrite structures. Further, "bainite" is a structure including cementite and other carbides between ferrite laths or including cementite and other carbides inside ferrite laths when observing thin  
35 film by a transmission type electron microscope. On the other hand, "bainitic ferrite and acicular ferrite



structures" means structures not including carbides inside ferrite laths and between ferrite laths other than Ti and Nb carbides.

Further, unavoidable martensite and residual austenite and pearlite may be included, but to secure good burring, the volume fraction of the residual austenite and martensite combined is preferably less than 5%. Further, to secure good fatigue characteristics, a volume fraction of pearlite including rough carbides is preferably 5% or less. Further, here, the volume fractions of ferrite, bainite, residual austenite, pearlite, and martensite are defined as the area fractions of the microstructure at 1/4 sheet thickness when polishing a sample cut out from a 1/4W or 3/4W position of the thickness of the steel sheet at the cross-section in the rolling direction, etching it with a Nital reagent, and observing it using an optical microscope at a power of X200 to X500.

Next, the reasons for limitation of the chemical ingredients of the present invention will be explained.

C is one of the most important elements in the present invention. That is, C clusters or precipitates with Mo or Cr even in welding or another short thermal cycle and suppresses softening of the weld heat affected zone as an effect. However, if contained in an amount over 0.1%, the workability and weldability deteriorate, so the amount is made 0.1% or less. Further, if less than 0.01%, the strength falls, so the amount is made 0.01% or more.

Si is effective for raising the strength as a solution strengthening element. To obtain the desired strength, 0.01% or more is required. However, if contained in an amount over 2%, the workability deteriorates. Therefore, the content of Si is made 0.01% to 2% or less.

Mn is effective for raising the strength as a solution strengthening element. To obtain the desired

strength, 0.05% or more is required. Further, when Ti and other elements besides Mn suppressing the occurrence of hot cracking due to S are not sufficiently added, addition, by wt%, of an amount of Mn giving  $Mn/S \geq 20$  is preferable. On the other hand, if adding over 3%, slab cracking occurs, so 3% or less.

P is an impurity and is preferably as low as possible. If contained in an amount over 0.1%, it has a detrimental effect on the workability and weldability and causes a drop in the fatigue characteristics as well, so is made 0.1% or less. S, if too great in content, causes cracking at the time of hot rolling, so should be reduced as much as possible, but 0.3% or less is an allowable range.

Al has to be added in an amount of 0.005% or more for deoxidation of the molten steel, but invites a rise in cost, so its upper limit is made 1%. Further, if added in too large an amount, it causes nonmetallic inclusions to increase and the elongation to deteriorate, so preferably the amount is made 0.5% or less.

N forms precipitates with Ti and Nb at higher temperatures than C and causes a reduction in the Ti and Nb effective for fixing the desired C. Therefore, it should be reduced as much as possible, but 0.005% or less is an allowable range.

Ti is one of the most important elements in the present invention. That is, Ti contributes to the rise in strength of the steel sheet due to precipitation strengthening. However, with less than 0.05%, this effect is insufficient, while even if contained in over 0.5%, not only is the effect saturated, but also a rise in the alloy cost is incurred. Therefore, the content of Ti is made 0.05% to 0.5%. Further, to fix by precipitation the C causing cementite or other carbides causing burring to deteriorate so as to improve the burring, it is necessary to meet the condition  $C - (12/48Ti - 12/14N - 12/32S) \leq 0.05\%$ . On the other hand, from the viewpoint of suppression of

softening of the weld heat affected zone, enough solid solution C for causing Mo or Cr to cluster or precipitate is required, so  $0 < C - (12/48Ti - 12/14N - 12/32S)$  is set.

Mo and Cr are some of the most important elements in the present invention. Even in welding or other short thermal cycles, they cluster or precipitate with C and other elements to suppress softening of the heat affected zone. However, if the total of the contents of Mo and Cr is less than 0.2%, the effect is lost. Further, even if contained in amounts over 0.5%, the effect is saturated, so  $Mo \leq 0.5\%$  and  $Cr \leq 0.5\%$  are set.

Nb contributes to the rise in strength of the steel sheet due to precipitation strengthening in the same way as Ti. However, with less than 0.01%, this effect is insufficient, while even if contained in an amount over 0.5%, not only does the effect become saturated, but also a rise in the alloy cost is incurred. Therefore, the content of Nb is made 0.01% to 0.5%. Further, it is necessary to fix by precipitation the C causing cementite and other carbides causing deterioration of the burring and therefore to satisfy the condition  $C - (12/48Ti + 12/93Nb - 12/14N - 12/32S) \leq 0.05\%$ . On the other hand, from the viewpoint of suppression of softening of the weld heat affected zone, enough solid solution C for causing the Mo or Cr to cluster or precipitate is needed, so  $0 < C - (12/48Ti + 12/93Nb - 12/14N - 12/32S)$  is set.

Ca and REMs are elements changing the forms of the nonmetallic inclusions forming starting points of cracking or causing deterioration of the workability to make them harmless. However, even if added in amounts of less than 0.005%, there is no effect, while if adding Ca in an amount of more than 0.02% and a REM in an amount of more than 0.2%, the effect is saturated, so addition of Ca in an amount of 0.005 to 0.02% and a REM in an amount of 0.005 to 0.2% is preferable.

Cu has the effect of improving the fatigue characteristics in the solid solution state. However,

with less than 0.2%, the effect is small, while if included in an amount over 1.2%, it precipitates during coiling and precipitation strengthening causes the steel sheet to remarkably rise in static strength, so the workability is seriously degraded. Further, in such Cu precipitation strengthening, the fatigue limit does not rise as much as the rise in the static strength, so the fatigue limit ratio ends up falling. Therefore, the content of Cu is made 0.2 to 1.2% in range.

Ni is added in accordance with need to prevent hot embrittlement due to the Cu content. However, if less than 0.1%, the effect is small, while if added in an amount of over 1%, the effect is saturated, so this is made 0.1 to 1%.

B has the effect of suppressing the granular embrittlement due to P believed to be caused by the reduction in the amount of solid solution C and therefore of raising the fatigue limit, so is added in accordance with need. Further, when the matrix strength is 640 MPa or more, a location in the weld heat affected zone receiving a thermal history of  $\alpha \rightarrow \gamma \rightarrow \alpha$  transformation has a low  $C_{ep}$ , so is not hardened and is liable to soften. In this case, by adding B for improving the hardenability, the softening at that location is suppressed. There is the effect that the fracture behavior of the joint is shifted from the weld zone to the matrix, so this is added in accordance with need. However, addition of less than 0.0002% is insufficient for obtaining these effects, while addition of over 0.002% causes slab cracking. Accordingly, B is added in an amount of 0.0002% to 0.002%.

Further, to impart strength, it is also possible to add one or two or more types of V and Zr precipitation strengthening or solution strengthening elements.

However, with less than 0.02% and 0.02%, respectively, this effect cannot be obtained. Further, even if added in amounts over 0.2% and 0.2% respectively, the effect is

saturated.

Note that the steel having these as main ingredients may also contain Sn, Co, Zn, W, and Mg in a total of 1% or less. However, Sn is liable to cause defects at the  
5 time of hot rolling, so 0.05% or less is preferable.

Next, the reasons for limitation of the method of production of the present invention will be explained in detail below.

The present invention can be obtained as cast, hot  
10 rolled, then cooled; as hot rolled; as hot rolled, then cooled, pickled, cold rolled, then heat treated; or as hot rolled steel sheet or cold rolled steel sheet heat treated by a hot dip line; and further as these steel sheets given separate surface treatment.

15 The method of production preceding the hot rolling in the present invention is not particularly limited. That is, after melting in a blast furnace or electric furnace etc., it is sufficient to perform various types of secondary refining to adjust the ingredients to give  
20 the target contents of ingredients, then cast this by the usual continuous casting, casting by the ingot method, thin slab casting, or another method. For the material, scrap may also be used. In the case of a slab obtained by continuous casting, the slab may be directly conveyed as  
25 a hot slab to the hot rolling mill or may be cooled to room temperature, then reheated in a heating furnace, then hot rolled.

The reheating temperature is not particularly limited, but if 1400°C or more, the scale off becomes  
30 large and the yield falls, so the reheating temperature is preferably less than 1400°C. Further, heating at less than 1000°C seriously detracts from the operational efficiency in schedules, so the reheating temperature is preferably 1000°C or more. Further, heating at less than  
35 1100°C not only results in precipitates including Ti and/or Nb not redissolving in the slab, but roughening

and causing a loss of the precipitation strengthening, but also the precipitates including Ti and/or Nb in the sizes and distributions desirable for burring no longer precipitate, so the reheating temperature is preferably 1100°C or more.

The hot rolling process comprises rough rolling, then finish rolling, but after rough rolling or after its succeeding descaling, it is also possible to bond a sheet bar and consecutively finish roll it. At that time, it is also possible to coil a rough bar once into a coil shape, store it in a cover having a heat retaining function in accordance with need, again uncoil it, then bond it. Further, the subsequent finish rolling is preferably performed within 5 seconds so as to prevent the formation of scale again after descaling.

The finish rolling has to end in a temperature region where the final pass temperature (FT) is the  $Ar_3$  transformation point + 30°C or more. This is because to obtain the bainitic ferrite or ferrite and bainite desirable for burring in the cooling process after the hot rolling, the  $\gamma \rightarrow \alpha$  transformation must occur at a low temperature, but in a temperature region where the final pass temperature (FT) is less than the  $Ar_3$  transformation point + 30°C, stress induced ferrite transformation nuclei are formed and polygonal coarse ferrite is liable to end up being produced. The upper limit of the finish temperature does not have to be particularly set so far as obtaining the effects of the present invention, but there is a possibility of occurrence of scale defects in operation, so making it 1100°C or less is preferable. Here, the  $Ar_3$  transformation point temperature is simply shown in relation with the steel ingredients by for example the following calculation formula:

$$Ar_3 = 910 - 310 \times \%C + 25 \times \%Si - 80 \times \%Mn$$

After the finish rolling ends, the steel is cooled to the designated coiling temperature (CT). The time

until the start of cooling is made within 10 seconds. This is because if the time until the start of cooling is over 10 seconds, right after rolling, the steel is liable to recrystallize and the austenite grains to end up becoming coarser and the ferrite grains after the  $\gamma \rightarrow \alpha$  transformation are liable to become coarser. Next, the average cooling rate until the end of cooling has to be at least 50°C/sec. This is because if the average cooling rate until the end of cooling is less than 50°C/sec, the volume fraction of the bainitic ferrite or ferrite and bainite desirable for burring is liable to end up decreasing. Further, the upper limit of the cooling rate is made 500°C/sec or less considering the actual capabilities of plant facilities. The cooling end temperature has to be in the temperature region of 700°C or less. This is because if the cooling end temperature is over 700°C, a microstructure other than the bainitic ferrite or ferrite and bainite desirable for burring is liable to end up being formed. The lower limit of the cooling end temperature does not have to be particularly defined to obtain the effect of the present invention. However, the coiling temperature or less is impossible in view of the process of the present invention. The processes from after cooling ends to coiling are not particularly defined, but in accordance with need, it is possible to cool to the coiling temperature, but in this case springback of the sheet due to thermal stress is a concern, so 300°C/sec or less is preferable.

Next, with a coiling temperature of less than 350°C, sufficient precipitates containing Ti and/or Nb are no longer formed and a drop in strength is feared, while if over 650°C, the precipitates containing Ti and/or Nb become coarser in size and not only no longer contribute to the rise in strength by precipitation strengthening, but if the precipitates become too large, voids will easily occur at the interface between the precipitates

and the matrix phase and the burring is liable to drop. Therefore, the coiling temperature is made 350°C to 650°C. Further, the cooling rate after coiling is not particularly limited, but when adding Cu in an amount of 1% or more, if the coiling temperature (CT) is over 450°C, Cu will precipitate after coiling and the workability will deteriorate. Not only this, the solid solution state Cu effective for improving the fatigue resistance is liable to be lost, so when the coiling temperature (CT) exceeds 450°C, the cooling rate after coiling is preferably at least 30°C/sec until 200°C.

After the end of the hot rolling process, in accordance with need, the steel is pickled, then may be processed in-line or off-line by skin pass rolling with a reduction ratio of 10% or less or cold rolling until a reduction ratio of 40% or so.

Next, when the cold rolled steel sheet is the final product, the hot finish rolling conditions are not particularly limited. Further, the final pass temperature (FT) of the finish rolling may be less than the  $A_{r3}$  transformation point temperature, but in this case a strong worked structure remains before the rolling or during the rolling, so restoration and recrystallization are preferable in the following coiling or heat treatment. The cold rolling process after the following pickling is not particularly limited for obtaining the effect of the present invention.

The heat treatment of this cold rolled steel sheet assumes a continuous annealing process. First, this is performed at a temperature region of 800°C or more for 5 to 150 seconds. When this heat treatment temperature is less than 800°C, in the later cooling, the bainitic ferrite or ferrite and bainite desirable for burring are liable not to be obtained, so the heat treatment temperature is made 800°C or more. Further, the upper limit of the heat treatment temperature is not



particularly defined, but due to restrictions of the continuous annealing facilities, is substantially 900°C or less.

On the other hand, a holding time at this temperature region of less than 5 seconds is insufficient for the Ti and Nb carbides to completely redissolve. Even with over 150 seconds of heat treatment, not only is the effect saturated, but also the productivity is lowered, so the holding time is made 5 to 150 seconds.

Next, the average cooling rate until the end of cooling has to be 50°C/sec or more. This is because if the average cooling rate until the end of cooling is less than 50°C/sec, the volume fraction of the bainitic ferrite or ferrite and bainite desirable for burring is liable to end up falling. Further, the upper limit of the cooling rate, considering the capabilities of actual plant facilities etc. is 200°C/sec or less.

The cooling end temperature has to be in the temperature region of 700°C or less, but when using a continuous annealing facility, the cooling end temperature usually never exceeds 550°C, so no special consideration is required. Further, the lower limit of the cooling end temperature does not have to be particularly set to obtain the effect of the present invention.

Further, after this, if necessary, skin pass rolling can be applied.

To coat with zinc the hot rolled steel sheet after pickling or said cold rolled steel sheet after the heat treatment process, the sheet may be dipped in a zinc coating bath. It may also be alloyed in accordance with need.

#### EXAMPLES

Below, examples will be used to further explain the present invention.

Each of the steels A to M having the chemical

ingredients shown in Table 1 was melted in a converter, continuously cast, reheated at the heating temperature shown in Table 2, rough rolled, then finish rolled to a thickness of 1.2 to 5.5 mm, then coiled. Note that the chemical compositions in the tables are expressed in wt%. Note that as shown in Table 2, some steels were pickled, cold rolled, and heat treated after the hot rolling process. The sheet thicknesses were 0.7 to 2.3 mm. On the other hand, among said steel sheets, the steel H and steel C-7 were zinc coated.

Details of the production conditions are shown in Table 2. Here, "SRT" indicates the slab heating temperature, "FT" the final pass finish rolling temperature, "start time" the time from the end of rolling to the start of cooling, "cooling rate" the average cooling rate from the start of cooling to the end of cooling, and "CT" the coiling temperature. However, when rolling later by cold rolling, the steels are not limited in this way, so "-" is indicated.

The tensile test for each of the thus obtained hot rolled sheets was conducted, as shown in FIG. 3(a) and FIG. 3(b), by first working the sheet to a No. 5 test piece described in JIS Z 2201, then following the test method described in JIS Z 2241. In FIG. 3(a) (plan view) and FIG. 3(b) (side view), 1 and 2 indicate steel sheets (test pieces), 3 a weld metal, 4 a joint, and 5 and 6 auxiliary sheets. Table 2 shows the yield point (YP), tensile strength (TS), and elongation at break (El). On the other hand, burring was evaluated by the burring test method described in the Japan Iron and Steel Federation standard JFS T 1001-1996. Table 2 shows the burring rate ( $\lambda$ ). Here, the volume fractions of ferrite, bainite, residual austenite, pearlite, and martensite are defined as the area fractions of the microstructure at 1/4 sheet thickness when polishing a sample cut out from a 1/4W or 3/4W position of the thickness of the steel sheet at the cross-section in the rolling direction, etching it with a

Nytaal reagent, and observing it using an optical microscope at a power of X200 to X500.

Further, a weld joint tensile test piece shown in FIG. 3 was used to conduct a tensile test by a method based on JIS Z 2241. The fracture locations were classified as matrix/weld zone by visual observation of the appearance. From the viewpoint of the joint strength, the weld fracture location is more preferably the matrix than the weld zone.

Note that the hardness of the weld heat affected zone of arc welding was measured by a No. 1 test piece described in JIS Z 3101 based on the test method described in JIS Z 2244. Note that the arc welding was performed with a shield gas of CO<sub>2</sub>, a wire of YM-60C,  $\phi$ 1.2 mm or YM-80C,  $\phi$ 1.2 mm made by Nippon Steel Welding Products and Engineering Co., Ltd., a welding rate of 100 cm/min, a welding current of 260 $\pm$ 10A, a welding voltage of 26 $\pm$ 1V, a thickness of the test material of 2.6 mm, a hardness measurement position of 0.25 mm from the surface, a measurement distance of 0.5 mm, and a test force of 98N.

The steels in accordance with the present invention were the nine steels of the steels A, B, C-1, C-7, F, H, K, L, and M. These gave high burring, high strength steel sheet excellent in softening resistance of the weld heat affected zone containing the predetermined amounts of steel ingredients and having microstructures comprised of ferrite or ferrite and bainite. Therefore, significant differences were recognized with respect to the heat affected zone softening degree  $\Delta H_v$  of 50 or more of the conventional steels evaluated by the method described in the present invention. Further, for the steel F, due to the effect of the addition of B, the hardenability was improved at the locations of the weld heat affected zone where  $\alpha$ - $\gamma$ - $\alpha$  transformation occurred. As a result, the fracture location became the matrix.

“ The other steels are outside the scope of the present invention due to the following reasons. That is, the steel C-2 had a finish rolling end temperature (FT) outside the scope of claim 8 of the present invention, so the desired microstructure described in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-3 had a time from the end of finish rolling to the start of cooling outside the scope of claim 8 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-4 had an average cooling rate outside the scope of claim 8 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-5 had a cooling end temperature and coiling temperature outside the scope of claim 8 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-6 had a coiling temperature outside the scope of claim 8 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-8 had a heat treatment temperature outside the scope of claim 9 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel C-9 had a holding time outside the scope of claim 9 of the present invention, so the target microstructure set forth in claim 1 could not be obtained and sufficient burring ( $\lambda$ ) could not be obtained. The steel D had a C\* outside the scope of claim 1 or 2 of the present invention, so the softening degree of the heat affected zone ( $\Delta H_v$ ) was large. The steel E had a C\* outside the scope of claim 1 or 2 of the present invention, so the softening degree of the heat affected

zone ( $\Delta H_v$ ) was large. The steel E had an amount of C added and C and C\* outside the scope of claim 1 or 2 of the present invention, so the softening degree of the heat affected zone ( $\Delta H_v$ ) was large. The steel G had an amount of Mo+Cr outside the scope of claim 1 of the present invention, so the softening degree of the heat affected zone ( $\Delta H_v$ ) was large. The steel I had an amount of Mo+Cr outside the scope of claim 1 of the present invention, so the softening degree of the heat affected zone ( $\Delta H_v$ ) was large. The steel J had a C\* outside the scope of claim 1 or 2 of the present invention, so the softening degree of the heat affected zone ( $\Delta H_v$ ) was large.

Table 1

Steel	Chemical composition (unit: wt%)														Remarks
	C	Si	Mn	P	S	Al	N	Ti	Nb	Mo	Cr	Mo+Cr	C*	Others	
A	0.063	0.03	0.51	0.005	0.0008	0.031	0.0028	0.089	0.036	0.11	0.10	0.210	0.039		Invention
B	0.082	1.60	2.10	0.084	0.0010	0.015	0.0033	0.131	0.041	0.10	0.12	0.220	0.047	Ca:0.0011	Invention
C	0.055	0.91	1.33	0.005	0.0011	0.035	0.0026	0.122	0.032		0.30	0.300	0.023		Invention
D	0.024	1.02	1.41	0.010	0.0010	0.022	0.0022	0.110	0.035	0.26		0.260	-0.006		Comparative
E	0.120	1.02	1.36	0.008	0.0007	0.024	0.0045	0.060			0.21	0.210	0.109		Comparative
F	0.052	0.88	1.35	0.018	0.0020	0.018	0.0028	0.116		0.22		0.220	0.026	B:0.0003	Invention
G	0.061	0.87	1.29	0.007	0.0011	0.022	0.0042	0.114	0.031			0.000	0.033		Comparative
H	0.053	0.86	1.41	0.007	0.0012	0.031	0.0031	0.112	0.025	0.25		0.250	0.025	Cu:0.8, Ni:0.3	Invention
I	0.058	0.94	1.28	0.003	0.0070	0.022	0.0038	0.121	0.038			0.000	0.029		Comparative
J	0.088	0.78	1.16	0.011	0.0009	0.031	0.0039	0.103		0.16	0.21	0.370	0.066		Comparative
K	0.060	0.90	1.40	0.007	0.0010	0.036	0.0045	0.121	0.019	0.20	0.09	0.290	0.032	REM:0.0008	Invention
L	0.035	1.10	1.51	0.006	0.0008	0.036	0.0018	0.091			0.32	0.320	0.014		Invention
M	0.033	1.12	1.31	0.006	0.008	0.036	0.0034	0.096		0.26		0.260	0.012	Cu:0.3	Invention

Table 2

Steel Class		Production conditions										Mechanical properties										Heat affected zone		Joint tensile fracture behavior	Remarks
		Hot rolling process					Cold rolling, heat treat. processes					Microstructure					Mechanical properties								
		SRT (°C)	FT (°C)	Ar <sub>3</sub> +30 (°C)	Start time (s)	Cooling rate (°C/s)	Cooling end temp. (°C)	Coiling temp. (°C)	Heat treat. temp. (°C)	Holding time (s)	Ferrite (%)	Bainite (%)	Other (%)	YP (MPa)	TS (MPa)	El (%)	λ (%)	Wire	ΔHv (98N)						
A	HR	1230	960	880	5	70	680	500	-	-	100	0	0	542	603	27	147	YM-28	-10	Matrix	Inv.				
B	HR	1230	910	787	5	70	680	500	-	-	90	10	0	906	1011	16	61	YM-80C	40	Weld zone	Inv.				
C-1	HR	1230	950	839	5	70	680	500	-	-	100	0	0	716	796	23	110	YM-60C	25	Weld zone	Inv.				
C-2	HR	1230	800	839	5	50	680	500	-	-	80	10	10	680	774	23	55	YM-60C	30	Weld zone	Comp.				
C-3	HR	1230	950	839	12	70	680	500	-	-	80	15	5	677	763	24	46	YM-60C	20	Weld zone	Comp.				
C-4	HR	1230	950	839	5	10	680	500	-	-	60	10	30	570	740	22	35	YM-60C	20	Weld zone	Comp.				
C-5	HR	1230	950	839	5	70	740	700	-	-	70	10	20	523	748	24	40	YM-60C	25	Weld zone	Comp.				
C-6	HR	1230	950	839	5	70	680	150	-	-	75	5	20	622	846	25	33	YM-60C	40	Weld zone	Comp.				
C-7	CR	-	-	-	-	-	-	-	850	120	100	0	0	700	801	20	87	YM-60C	20	Weld zone	Inv.				
C-8	CR	-	-	-	-	-	-	-	750	120	70	30	0	542	733	21	26	YM-60C	40	Weld zone	Comp.				
C-9	CR	-	-	-	-	-	-	-	850	1	100	0	0	791	861	6	30	YM-60C	55	Weld zone	Comp.				
D	HR	1180	900	845	7	60	700	600	-	-	100	0	0	697	774	22	120	YM-60C	90	Weld zone	Comp.				
E	HR	1180	910	820	7	60	700	600	-	-	70	30	0	780	885	19	35	YM-60C	30	Weld zone	Comp.				
F	HR	1180	920	838	7	60	700	600	-	-	100	0	0	710	789	22	105	YM-60C	15	Matrix	Inv.				
G	HR	1180	910	840	7	60	700	600	-	-	100	0	0	714	793	22	100	YM-60C	70	Weld zone	Comp.				
H	HR	1180	930	832	7	60	700	600	-	-	100	0	0	706	797	20	82	YM-60C	20	Weld zone	Inv.				
I	HR	1180	900	843	7	60	700	600	-	-	100	0	0	693	796	21	85	YM-60C	85	Weld zone	Comp.				
J	HR	1180	900	839	7	60	700	600	-	-	80	20	0	719	799	23	51	YM-60C	20	Weld zone	Comp.				
K	HR	1180	930	832	7	60	700	600	-	-	100	0	0	729	810	20	96	YM-60C	10	Weld zone	Inv.				
L	HR	1180	920	836	7	60	700	600	-	-	100	0	0	725	805	20	97	YM-60C	10	Weld zone	Inv.				
M	HR	1180	920	853	7	60	700	600	-	-	100	0	0	730	816	19	90	YM-60C	20	Weld zone	Inv.				

HR: Hot rolling, CR: cold rolling

INDUSTRIAL APPLICABILITY

As explained above in detail, the present invention relates to high burring, high strength steel sheet having a tensile strength of 540 MPa or more excellent in softening resistance of the weld heat affected zone and a method of production of the same. By use of such thin steel sheet, a great improvement can be expected in the softening resistance of the weld heat affected zone in the case of spot, arc, plasma, laser, or other welding after being formed or the case of being formed after such welding.